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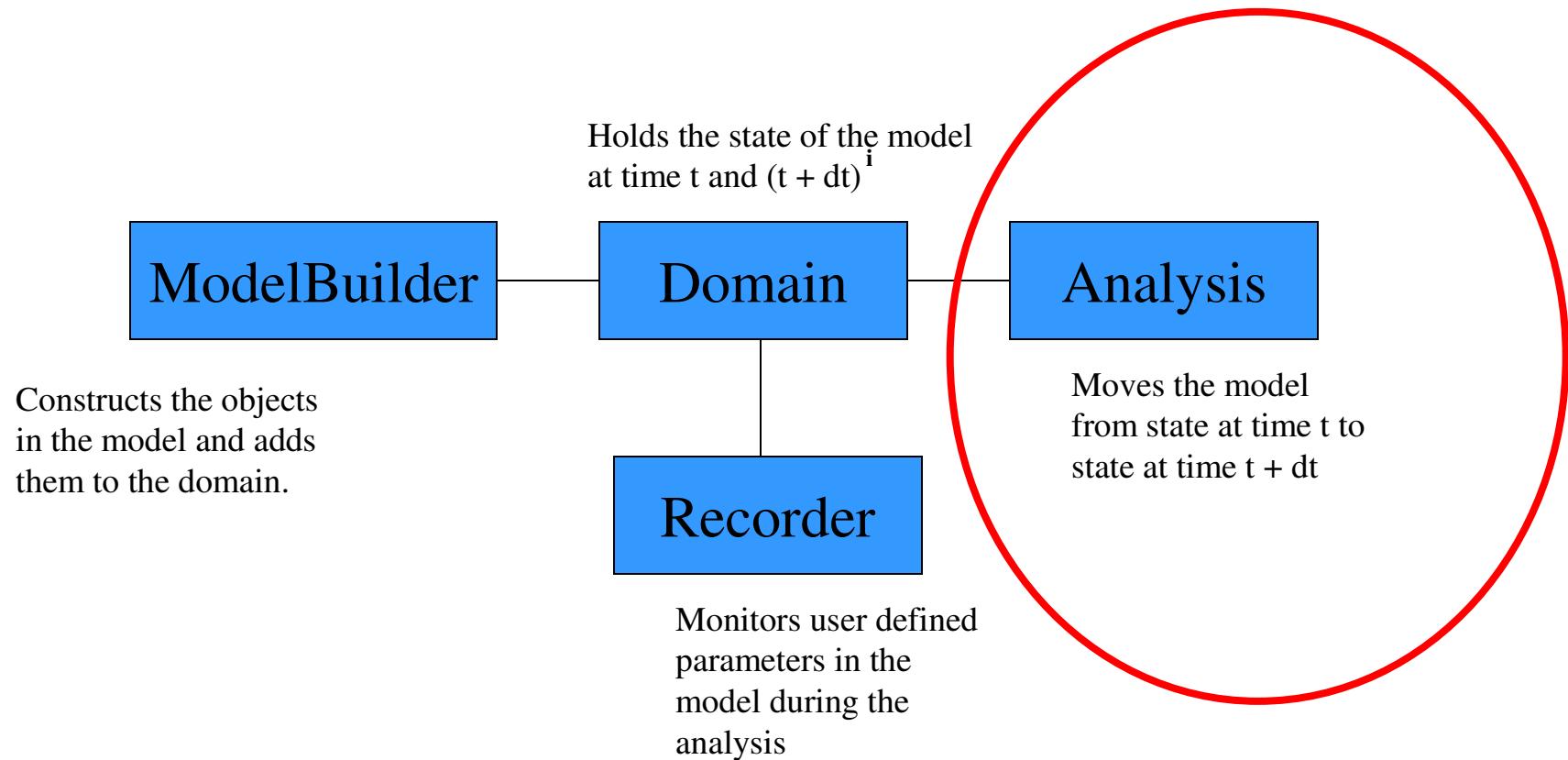
Introduction to Analysis Commands

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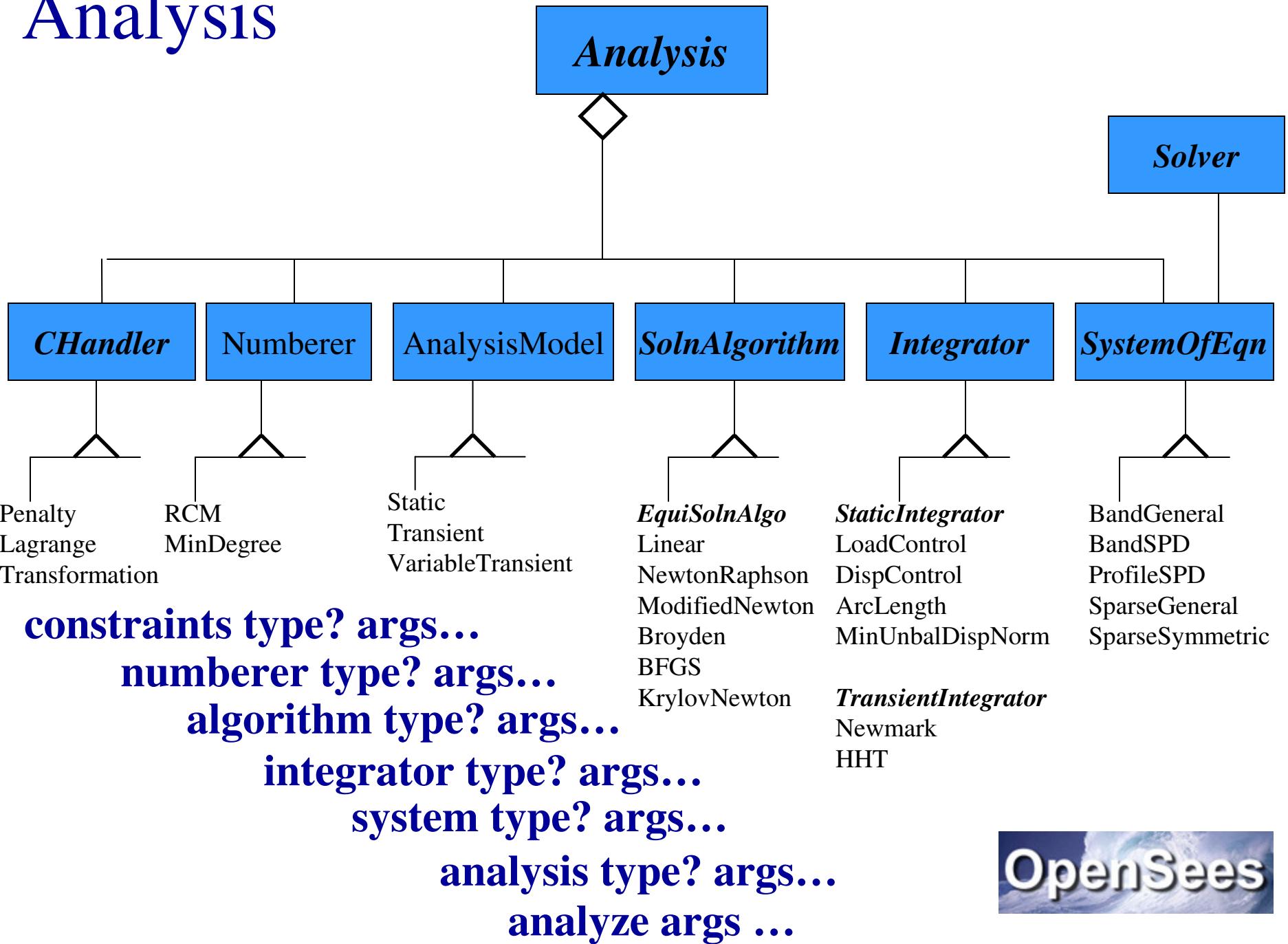
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Main Abstractions in OpenSees



In this presentation we focus on **ANALYSIS GENERATION**

Analysis

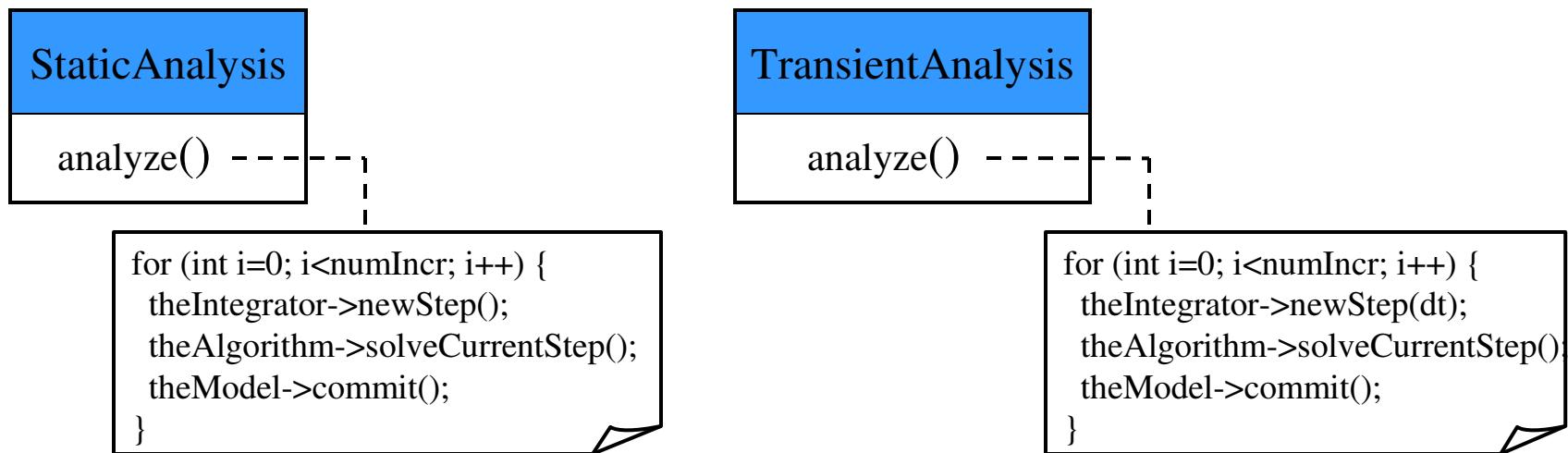


analysis command:

- Static Analysis
- Transient Analysis
 - both incremental solution strategies

analysis static

analysis transient



- Eigenvalue
 - general eigenvalue problem
 $(\mathbf{K} - \lambda \mathbf{M})\Phi = 0$
 - standard eigenvalue problem
 $(\mathbf{K} - \lambda)\Phi = 0$

eigen numModes? -general

eigen numModes? -standard

integrator command:

- determines the predictive step for time $t+\delta t$
- specifies the tangent matrix and residual vector at any iteration
- determines the corrective step based on ΔU

- Transient Integrator for Use in Transient Analysis

Nonlinear equation of the form:

$$R(U, \dot{U}, \ddot{U}) = P(t) - F_I(\ddot{U}) - F_R(U, \dot{U})$$

- Newmark Method

integrator Newmark $\gamma\beta$

- Hilbert-Hughes-Taylor Method

integrator Newmark α

- Static Integrators for Use in Static Analysis

Nonlinear equation of the form:

$$\mathbf{R}(\mathbf{U}, \lambda) = \lambda \mathbf{P}^* - \mathbf{F}\mathbf{R}(\mathbf{U})$$

- Load Control

$$\lambda_n = \lambda_{n-1} + \Delta\lambda$$

integrator LoadControl Δλ

*does not require a reference load, i.e. loads in load patterns with Linear series and all other loads constant.

- Displacement Control

$$\mathbf{Uj}_n = \mathbf{Uj}_{n-1} + \Delta\mathbf{Uj}$$

integrator DisplacementControl node dof Δλ

- Arc Length

$$\Delta\mathbf{U}_n^\top \Delta\mathbf{U}_n + \alpha^2 \Delta\lambda_n = \Delta s^2$$

integrator LoadControl α Δs

- Minimum Unbalance Displacement Norm

$$\frac{d}{d\Delta\lambda} (\Delta\mathbf{U}_n^\top \Delta\mathbf{U}_n) = 0$$

integrator LoadControl Δλ

algorithm command:

- to specify the steps taken to solve the nonlinear equation

- Linear Algorithm

```
theIntegrator->formUnbalance();
theIntegrator->formTangent();
theSOE->solve()
theIntegrator->update(theSOE->getX());
```

algorithm Linear

- Newton-Raphson Algorithm

```
theIntegrator->formUnbalance();
do {
    theIntegrator->formTangent();
    theSOE->solve()
    theIntegrator->update(theSOE->getX());
    theIntegrator->formUnbalance();
} while (theTest->test() == fail)
```

algorithm Newton

- Modified Newton Algorithm

algorithm ModifiedNewton <-initial>

- Accelerated Modified Newton Algorithm

algorithm KrylovNewton <-initial>

constraints command:

- to specify how the constraints are enforced

$$\mathbf{U}_c = \mathbf{C}_{rc} \mathbf{U}_r$$

$$\mathbf{C} \mathbf{U} = \mathbf{0}$$

$$\mathbf{T} \mathbf{U}_r = [\mathbf{U}_r \ \mathbf{U}_c]^\wedge$$

$$[\mathbf{C}_r \ \mathbf{C}_c]^\wedge [\mathbf{U}_r \ \mathbf{U}_c] = \mathbf{0}$$

- Transformation Handler

$$\mathbf{K}^* \mathbf{U}_r = \mathbf{R}^*$$

$$\mathbf{K}^* = \mathbf{T}^\wedge \mathbf{K} \mathbf{T}$$

$$\mathbf{R}^* = \mathbf{T}^\wedge \mathbf{R}$$

constraints Transformation

in OpenSees currently don't allow retained node in one constraint to be a constrained node in another constraint

- Lagrange Handler

$$\begin{bmatrix} \mathbf{K} & \mathbf{C}^\wedge \\ \mathbf{C} & 0 \end{bmatrix} \begin{bmatrix} \mathbf{U} \\ \lambda \end{bmatrix} = \begin{bmatrix} \mathbf{R} \\ \mathbf{Q} \end{bmatrix}$$

constraints Lagrange

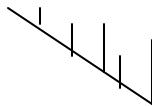
- Penalty Handler

$$[\mathbf{K} + \mathbf{C}^\wedge \alpha \mathbf{C}] \mathbf{U} = [\mathbf{R} + \mathbf{C}^\wedge \alpha \mathbf{Q}]$$

constraints Penalty α_{sp} ? α_{mp} ?

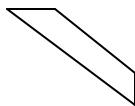
system command:

- to specify how matrix equation $KU = R$ is stored and solved
- Profile Symmetric Positive Definite (SPD)



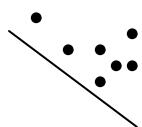
system ProfileSPD

- Banded Symmetric Positive Definite



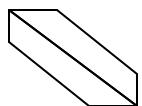
system BandSPD

- Sparse Symmetric Positive Definite



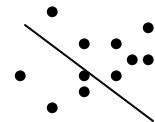
system SparseSPD

- Banded General



system BandGeneral

- Sparse Symmetric



system SparseGeneral

system Umfpack

numberer command:

- to specify how the degrees of freedom are numbered

- Plain Numberer

nodes are assigned dof arbitrarily

numberer Plain

- Plain Numberer

nodes are assigned dof using the
Reverse Cuthill-McKee algorithm

numberer RCM

test command:

- to specify when convergence has been achieved

all look at system: **KU = R**

- Norm Unbalance

$$\sqrt{\mathbf{R}^T \mathbf{R}} < \text{tol}$$

test NormUnbalance tol? numIter? <flag?>

- Norm Displacement Increment

$$\sqrt{\mathbf{U}^T \mathbf{U}} < \text{tol}$$

test NormDispIncr tol? numIter? <flag?>

- Norm Energy Increment

$$\frac{1}{2} (\mathbf{U}^T \mathbf{R}) < \text{tol}$$

test NormEnergyIncr tol? numIter? <flag?>

- Relative Tests

test RelativeNormUnbalance tol? numIter? <flag?>

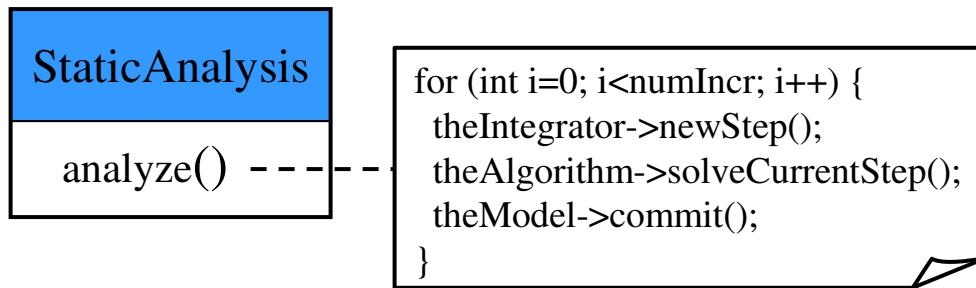
test RelativeNormDispIncr tol? numIter? <flag?>

test RelativeNormEnergyIncr tol? numIter? <flag?>

analyze command:

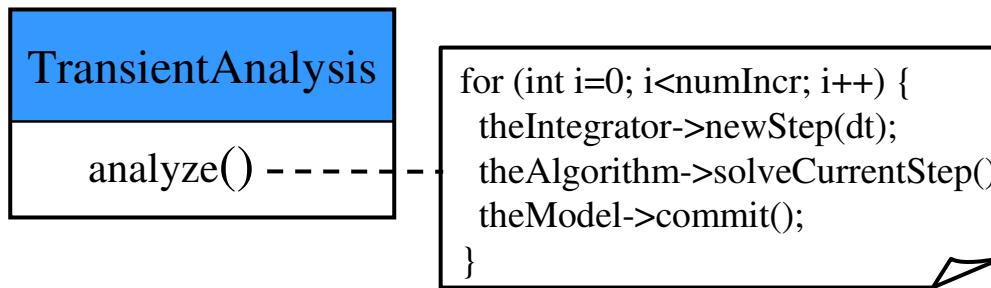
- to perform the static/transient analysis

- Static Analysis



analyze numIter?

- Transient Analysis



analyze numIter? Δt?

Example Analysis:

- Static Nonlinear Analysis with LoadControl

```
constraints transformation
numberer RCM
system BandGeneral
test NormDispIncr 1.0e-6 6 2
algorithm Newton
integrator LoadControl 0.1
analysis Static
analyze 10
```

- Transient Nonlinear Analysis with Newmark

```
constraints transformation
numberer RCM
system BandGeneral
test NormDispIncr 1.0e-6 6 2
algorithm Newton
integrator Newmark 0.5 0.25
analysis Transient
analyze 2000 0.01
```

